# STONE DIKE ALTERATIONS PROJECT REPORT MIDDLE MISSISSIPPI RIVER, MILES 201-0 <br> (UMRS - EMP) ENVIRONMENTAL MANAGEMENT PROGRAM <br> REPORT UPDATE 

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## INTRODUCTION

For the purposes of this project, the Middle Mississippi River is defined as the reach from approximately Alton to Cairo, Illinois between Miles 201 and 0 . The 201-mile reach of river is relatively short compared to the more notable Upper and Lower Mississippi Rivers. The reach begins immediately upstream of Mel Price Lock and Dam and ends at the confluence with the Ohio River. Over 750 dikes and chevrons currently exist on the Middle Mississippi River for the purpose of maintaining adequate depths for navigation.

The Stone Dike Alterations Project was initiated under the Environmental Management Program by a fact sheet dated September 30, 1991. The project investigated the possibility of altering existing dikes to permit flow near channel borders at higher river stages which would result in more diverse scour and depositional patterns. The project outlined recommendations for areas where it was determined that the biological need for habitat alteration was the greatest and where the notching of existing dikes offered the greatest opportunity for success. As part of the project, a report was generated in 2002 focusing on an inventory of Middle Mississippi River parameters and the potential for structure alteration based on need for habitat enhancement and the possibility for enhancement. This report is intended to update the 2002 report, outlining changes in channel geometry, updating dike construction and notching locations, and providing new recommendations for channel enhancement. This report will also serve as a guide for possible pallid sturgeon habitat restoration activities in the Middle Mississippi River related to the District's Biological Opinion Program.

## OBJECTIVES

The objectives of this Stone Dike Alterations Project Report update follow:

1. Document the channel geometry and construction changes in each reach from 2002 to 2011.
2. Identify the repetitive maintenance dredging locations in each reach from 2002 to 2011.
3. Re-prioritize the reaches for modifications based on their initial ranking, changes within the reach, and other new additional information since the previous report.
4. Provide an updated description of the types and effects of structures currently designed and constructed within the district.
5. Coordinate with partnering agencies - US Fish and Wildlife Service, Illinois Department of Natural Resources, and Missouri Department of Conservation - to update where benefit is both possible and necessary.
6. Produce a finalized update detailing the changes in Middle Mississippi River parameters and needs for use in guiding future design decisions.

## MIDDLE MISSISSIPPI RIVER REACHES

The predecessor to this report identified the basic features of the Middle Mississippi River, which are largely unchanged. For convenience in comparison, the 22 individual sections (here on identified as reaches) were held constant from the 2002 report to this report. Physical descriptions and the parameters of each reach follow. The descriptions for each reach include: river miles, characteristics and configuration, water surface slope, average bank and navigation channel widths, total number of main channel structures, main channel structures per river mile, percent of main channel structures notched, bendway weir fields, side channels, side channel miles per river mile, dredging areas, priority ranking, and alteration possibilities. Tables and graphs that summarize this data for all the reaches are shown in Appendix A. Maps of each reach are located in Appendix B, Figures 1 to 22. These maps include: the navigation line, the channel contraction borders, river borders, dikes, chevrons, weirs, revetments, the 2010 bathymetry, dredge cuts and disposal sites between 2002 and 2011, 2011 aerial photography, and local reference annotation. The dikes whose identifier symbols have crosses are older structures that were not visible in low water aerial photographs from 2006. The green rectangles represent dredge cut sites and the red rectangles represent dredge disposal sites. Degraded structure indicated on the maps includes both natural and designed (i.e. constructed notches) degradation. Notches totaled below and in tables and charts in Appendix A are strictly designed notches.

The same system used for the prioritization of the reaches in the last report was used in this update. The reaches were prioritized to reflect the areas the team members felt were most critical and in need of environmental modifications. To prioritize the reaches, a rating system of one through five stars was used, with five stars being the highest priority. The rating for each reach was developed based on a combination of the need for additional habitat and biological enhancement and the probability of each reach achieving the goals set forth (i.e. a small number of dikes limits enhancement possibilities, industry opposition limits construction options, etc.). A secondary rating system was established to rate the specific fields along the same criteria of need and opportunity; the rankings used were high, medium, or low.

## GUIDANCE:

Bankline width includes width to the outer bank of chutes if present
Trail dikes and rootless dike extensions were counted as part of the main stem dike
Only main channel structures were included in dikes/mile calculation
Chute mile per channel mile length was calculated using estimated chute centerline
For the purpose of the dikes per mile calculation, chevrons were considered dikes; hardpoints were not

## REACH 1: MEL PRICE TAILWATER, 5 MILES (201 - 196)

Map: $\quad$ Appendix B, Figure 1
Characteristics: Straight from the Lock (Mile 201) to Mile 199, then a gradual 70-degree bend to the right to Mile 197, then straight to Mile 196. No bedrock controls or bluff lines.

Slope: Water Surface: 0.59 feet/mile
Avg Width: Bankline: 2080 ft
Nav. Channel: 1500 ft
Dikes: 2002:
3 Total Dikes on RDB (198.7 - 197.5)
0.6 dikes/mile - $0 \%$ Notched

These dikes consist of a hand-placed stone exterior with a sand filled interior. Therefore, modifications to these structures are not possible without adversely affecting the structural integrity of the entire dike

2011:
5 Main Channel Structures
5 Dikes on the RDB (199.4-197.7)
1.0 dikes/mile - $0 \%$ Notched

Some of these dikes (198.7 - 197.5) are known to consist of a hand-placed stone exterior with a sand filled interior. Therefore, modifications to these structures are not possible without adversely affecting the structural integrity of the entire dike.

Structure changes:
Two dikes discounted in the 2002 report were present in the low water aerial photography.

| Weirs: | None |
| :---: | :---: |
| Chutes: | 2002: |
|  | 0.60 miles/mile |
|  | Maple Island RDB (200.5 - 197.5) 3 closures (probably hand-placed stone and segments of the dikes on the located channel side) |
|  | 2006: |
|  | 0.60 miles/mile |
|  | Maple Island RDB (200.5 - 197.5) 4 closures (3 probably hand-placed stone and segments of the dikes on the located channel side) |
| Dredging: | 10 cuts, along the LDB (auxiliary lock chamber at Mel Price L\&D) for a total of 794,238 cubic yards (CY) |
| Priority: | 2002: |
|  | 1 Star. |
|  | 2011: |
|  | 1 Star. |

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\begin{array}{ll}\text { Conclusions: } & \begin{array}{l}\text { 2002: } \\
\text { Structural modifications are not possible due to the existing dikes being sand-filled. } \\
\text { Notches cut into these dikes may cause failure of the entire structure. }\end{array} \\
& \begin{array}{l}\text { 2011: } \\
\text { No change. }\end{array}
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REACH 2: \& MOSENTHEIN, 12 MILES (196 TO 184)\end{array}\right]\)| Map: | Appendix B, Figure 2 |
| :--- | :--- |

2006:
0.48 miles/mile

Duck Island RDB (195.3 - 193.8) 0 Closures
Mosenthein LDB (189 - 184.8) 1 Closure \& 6 Dikes within chute

Dredging: 17 cuts for a total of 1,594,767 CY:
5 cuts along the LDB at $\sim$ RM 196 for a total of 586,538 CY
7 cuts along the LDB at $\sim$ RM 194 at the entrance to the canal for a total of 691,518 CY
5 cuts along the LDB at $\sim$ RM 184 at the entrance to the canal for a total of 316,711 CY

Priority: 2002:
3 Stars.

2011:
3 Stars.

Conclusions: 2002:
The area is a transition point between the Middle Mississippi River and the Lower Missouri River. Therefore, the area may be an important staging area for sturgeon and other species. There are limited opportunities to improve habitat conditions in the St. Louis Harbor, located just downstream of this reach. Experimental structures or modifications may be tested in most of this reach due to the absence of a navigation channel. None of the existing dikes in this reach have been modified for environmental enhancement.

2011:
Changes in this area have been limited to weir restoration and the extension of the 184.2 L dike. Opportunities exist throughout the reach if there is interest although the habitat is already generally perceived as good. RM 196 continues to be a repetitive maintenance issue that may allow for a habitat-conducive remedy such as a chevron. No notching has been done on the LDB structures in the vicinity of Mosenthien Island. However, deposition in the old channel may limit ability for construction changes from RM 184 to 192.

## REACH 3: ST. LOUIS HARBOR, 16 MILES (184 TO 168)

Map: Appendix B, Figure 3
Characteristics: Long bend to the right between Miles 184 to 176, then a slight bend to the left to Mile 174, and then straight to Mile 168.
Minimal dikes located throughout reach due to the number of facilities along both banks. The bluff line is located along RDB throughout most of the reach.
6 Existing Bridges and 1 Planned Bridge crossing are between Miles 183.2 and 179.
Slope: Water Surface: 0.56 feet/mile

Avg Width Bankline: 2175 ft
Channel: 1406 ft


2011:

2 Stars. - Need being model with an HSR Model
Conclusions: 2002:
Additional structures absolutely must not affect navigation through this busy stretch of river, especially within the reach with 7 bridge crossings. The 5 existing structures in Dike Field 2 already have additional environmental modifications designed to create an island and side channel complex - see the Jefferson Barracks Micro Model Study Report M17. A portion of this design has already been constructed. No other opportunities exist due to the lack of navigation structures located in the reach.

2011:
Navigation concerns heavily dominate this reach, and thus limit bathymetric and environmental concerns. There have been efforts to include notching and chevrons into construction plans since the last report. A model study is currently ongoing (2012) of this reach and may present an opportunity for testing additional designs as part of navigation improvement work.

## REACH 4: CLIFF CAVE, 4.5 MILES (168 TO 163.5)

Map: $\quad$ Appendix B, Figure 4
Characteristics: Straight to Mile 165 and then a gradual 30-degree bend to Mile 163.5
The bluff line is located along the RDB
Slope: $\quad$ Water Surface: 0.55 feet/mile
Width Bankline: 2000 ft
Channel: $\quad 1350 \mathrm{ft}$
Dikes: 2002:
21 Total Dikes (12 RDB \& 9 LDB)
4.7 dikes/mile - $5 \%$ notched

Dike Field 1: LDB continuous ( 168 - 166) 6 Dikes around JB Chute
Dike Field 2: RDB continuous (166.5-163.5) 12 dikes, many D/S angled
Dike Field 3: LDB (165-164.5) 3 dikes, mainly stub or hard points
2011:
22 Main Channel Structures
12 Dikes along the RDB (166.4-163.7)
10 Dikes along the LDB (167.7-163.6)
4.9 dikes/mile - 14\% Notched

Structure Changes:
One dike ( 163.6 L) discounted in the 2002 report was present in the low water aerial photography. Two dikes (167.7 L, 167.4 L) were extended.

Weirs: 2002:
Carl Baer LDB (164-163.5) 6 Weirs
2011:

No change
Chutes: 2002:
0.27 miles/mile

Jefferson Barracks LDB (167.7-166.5) 1 closure
2006:
No change
Dredging: $\quad 9$ cuts in the center of the channel at $\sim$ RM 168 - RM 166.5 for a total of 1,349,713 CY
Priority: 2002:
4 Stars.
2011:
3 Stars. - Additional notching has occurred and constructability is an issue.
Conclusions: 2002:
This is a relatively short reach with only one small side channel. Possible modifications exist in dike fields $1 \& 2$. Modifications in field 1 and the upper part of field 2 may also have a secondary benefit of reducing maintenance dredging. Field 3 consists mainly of stub dikes.

2011:
Field 1 - High. Opportunities exist around Jefferson Barracks Chute and surrounding dikes. This field was a larger dredging issue in the past that is still active. Fleeting will be an issue.
Field 2 - Medium. There is limited opportunity for dike modification, but the potential for dike construction exists around the sand bar along the lower end of the field. Field 3 - Low. This is a short field with only three short dikes with fleeting in the vicinity.

## REACH 5: KIMMSWICK, 7 MILES (163.5-156.5)

Map: $\quad$ Appendix B, Figure 5
Characteristics: Relatively straight throughout the reach.
The bluff line is located along the RDB
The confluence with the Meramec River along the RDB is located at Mile 160.7R
Slope: Water Surface: 0.52 feet/mile
Width Bankline: 2371
Channel: 1271
Dikes: 2002:
26 Total Dikes (4 RDB \& 22 LDB)
3.7 dikes/mile - 4\% notched

Dike Field 1: LDB Continuous (163-156.5) 22 dikes
Dike Field 2: RDB Continuous (160-159) 4 dikes

2011:
34 Main Channel Structures
4 Dikes along RDB (159.8-158.9)
23 Dikes along the LDB ( 163 - 156.7)
7 Chevrons along the LDB (162.8-159.9)
4.9 dikes/mile - 3\% Notched

Structure Changes:
Four new dikes (162.1 L, 158.1 R, 157.7 R, 157.3 R) were constructed; the survey revealed a scour hole off the tip of three of the four dikes ( 157.7 R the lone exception). Seven chevrons were constructed. Four ( $162.5 \mathrm{~L}, 160.3 \mathrm{~L}, 160.0 \mathrm{~L}, 159.9 \mathrm{~L}$ ) of the seven chevrons that were constructed demonstrated scour hole development downstream. The three remaining chevrons were not constructed before the survey. One dike (161.9 L) was extended from the root.

Weirs: None
Chutes: 2002:
0.10 miles/mile

Atwood LDB (161.5-160.8) 1 closure
2006:
No change
Dredging: 19 cuts for a total of $1,945,141 \mathrm{CY}$ :
4 cuts in the center of the channel at $\sim$ RM 162.5 for a total of 277,571 CY
9 cuts along the RDB at RM 161.4 - RM 160.2 for a total of 952,776 CY
6 cuts in the center of the channel at RM 158.3 - RM 156.9 for a total of 714,794 CY
Priority: 2002:
4 Stars.
2011:
3 Stars. - Recent work needs to be evaluated.
Conclusions: 2002:
This is a relatively straight reach with only one small side channel. Possible modifications exist in both dike fields. More possibilities exist in dikes along LDB. A secondary benefit of reducing maintenance dredging may be incurred with modifications to the dikes adjacent to the mouth of the Meramec River. This confluence may contain important spawning habitat for sturgeon.

2011:
Field 1 - Low. Chevron construction and dike modification was recently completed in this field. The results of this work will be evaluated and the field reassessed in future years. Half of the chevrons built in this section exhibit the downstream scour that has been beneficial to habitat diversity.
Field 2 - Medium. Opportunities for modification in this field are limited, but the opportunity exists for island creation downstream of the field. There is a sensitivity issue with the locals in this area.

## REACH 6: HERCULANEUM, 7 MILES (156.5-149.5)

Map: $\quad$ Appendix B, Figure 6
Characteristics: Very straight reach with the bluff line along the RDB.
Slope: Water Surface: 0.46 feet/mile
Width Bankline: 1943
Channel: 1271
Dikes: 2002:
29 Total Dikes (12 RDB \& 17 LDB)
4.1 dikes/mile - $0 \%$ notched

Dike Field 1: LDB continuous (156.5-150) 17 dikes
Dike Field 2: RDB continuous (154-153) 4 dikes
Dike Field 3: RDB (151.8-151.3) 3 dikes
Dike Field 4: RDB continuous (150.6-149.5) 5 dikes
2011:
30 Main Channel Structures
18 Dikes along LDB (156.5-150)
12 Dikes along RDB (154-149.5)
4.3 dikes/mile - 3\% notched

Structure Changes:
One dike ( 150.3 L ) discounted in the 2002 report was present in the low water aerial photography. One dike (146.3 L) was notched.

Weirs: None
Chutes: 2002:
None - 0.0 miles/mile
2006:
No change.
Dredging: $\quad 4$ cuts along the LDB of the channel at $\sim$ RM 153 for a total of 142,380 CY
Priority: 2002
5 Stars.
2011:
5 stars.
Conclusions: 2002:
There are no side channels, the reach is straight, and none of the dikes have been modified for environmental enhancement. Because of the reduced contraction line, there are no dredging problems. Therefore, many possible modifications exist.

Field 1 - High. Herculaneum has a project plan developed and priced under NESP for chevrons and dike modifications as the Prototype Reach. It is awaiting funding. The situation remains the same.
Field 2 - High. Herculaneum has a project plan developed and priced under NESP for chevrons and dike modifications. It is waiting for funding. The situation remains the same.
Field 3 - Low. This is a short field with only three short dikes.
Field 4 - Low. This is a short field with only five short dikes.

## REACH 7: CALICO/OSBORNE, 6.5 MILES (149.5-143)

Map: $\quad$ Appendix B, Figure 7

Characteristics Straight to Mile 146 and then a gradual bend to the left then to the right to Mile 143. The bluff line is located along the RDB.

Slope: Water Surface: 0.49 feet/mile
Width Bankline: 2043
Channel: 1257

Dikes: 2002:
33 Total Dikes (15 RDB \& 18 LDB)
5.1 dikes/mile - 3\% notched

Dike Field 1: LDB continuous (149.5-143) 18 dikes
Dike Field 2: $\quad$ RDB sporadic $(149.5-146.3) 5$ dikes
Dike Field 3: $\quad$ RDB continuous (145.5-143) 10 dikes

2011:
32 Main Channel Structures
16 Dikes along RDB (149.3-143)
16 Dikes along the LDB (149.2 - 143.4)
4.9 dikes/mile - 6\% Notched

Structure Changes:
Two dikes (149.0 L, 146.25 L) identified in the 2002 report were not visible on the 2006 aerial photography. One dike (146.25 R) discounted in the 2002 report was present in the low water aerial photography. One dike (146.3 L) was notched.

Weirs: None

Chutes: 2011:
0.46 miles/mile

Calico LDB (148.3 - 147.3) 1 closure
Osborne LDB (146.3-144.3) 6 closures

2006:
0.46 miles/mile

Calico LDB (148.3 - 147.3) 2 closure (an additional closure was visible in the 2006 aerial photography)
Osborne LDB (146.3-144.3) 6 closures
Dredging: $\quad 2$ cuts in the center of the channel at $\sim$ RM 145.5 for a total of $96,056 \mathrm{CY}$
Priority: 2002:
2 Stars.
2011:
3 Stars. - Island creation poses modification opportunity.
Conclusions: 2002:
Two side channels currently exist in this reach. Because of the reduced contraction line, there are no dredging problems. Therefore, many possible modifications exist. Note: There may be issues with possible lead contamination in this reach.

2011:
Field 1 - High. Numerous opportunities exist for dike modification, and great opportunities exist for habitat complex creation around the chutes.
Field 2 - Low. This is a short field with only five short dikes.
Field 3 - High. Opportunities exist with the adjacent Harlow Island site. This area has been identified as a high priority site for island creation. Any modifications would likely be coupled with an EMP project at Harlow Island.

## REACH 8: $\quad$ SALT LAKE, 8.5 MILES (143 - 134.5)

Map: $\quad$ Appendix B, Figure 8
Characteristics: Relatively straight throughout the reach except for a slight bend between Miles 140 and 138. The bluff line is located along the RDB in the downstream portion of the reach.

Slope: $\quad$ Water Surface: 0.53 feet/mile
Width Bankline: 2688
Channel: 1388
Dikes: 2002:
37 Total Dikes (10 RDB \& 27 LDB)
4.4 dikes/mile - 8\% notched

Dike Field 1: LDB continuous (142.2-134.5) 27 dikes
Dike Field 2: RDB sporadic (142.5-139.5) 10 dikes, mainly stub
2011:
38 Main Channel Structures
11 Dikes along RDB (142.5-134.7)
27 Dikes along the LDB (142.2-134.8)
4.5 dikes/mile - 8\% notched

## Structure Changes:

One dike (134.7 R) discounted in the 2002 report was present in the low water aerial photography.

Weirs: None
Chutes: 2002:
0.35 miles/mile

Salt Lake LDB (139.5 - 136.5) 6 closures
2006:
No change.
Dredging: 1 cut in the center of the channel at $\sim$ RM 138.7 for a total of $34,551 \mathrm{CY}$
Priority: 2002:
3 Stars.
2011:
3 Stars.
Conclusions: 2002:
Although one large side channel currently exists in the reach, there is a general lack of diversity due to the relatively few number of dikes that have been notched. There are no dredging problems therefore many possible modifications exist. More possibilities exist in dike field 1 due to the number and length of these dikes. Dike modifications for the enhancement of Salt Lake Chute have been designed - see the Salt Lake Chute Micro Model Study Report M16.

2011:
Field 1- High. Opportunities exist in conjunction with work for habitat complex creation at Salt Lake Chute. This site has been proposed for studying with a model soon. Field 2 - Low. The dikes in this field are typically very short, and as such, any improvements would be on a dike-specific basis.

## REACH 9: FORT CHARTRES, 6.5 MILES (134.5-128)

Map: $\quad$ Appendix B, Figure 9
Characteristics: The reach consists of three consecutive bends. First there is a bend to the left, then to the right, then back to the left.

Slope: Water Surface: 0.55 feet/mile
Width Bankline: 2257
Channel: 1086
Dikes: 2002:
19 Total Dikes (6 RDB \& 13 LDB)
2.9 dikes/mile - 0\% notched

Dike Field 1: LDB continuous along Ft Chartres Island (134.5-132.5) 6 dikes
Dike Field 2: RDB along Establishment Island (132.5-130) 6 dikes
Dike Field 3: LDB continuous (130.5-128.5) 7 dikes, many stub

2011:
22 Main Channel Structures
6 Dikes along RDB (132.6-130.2)
2 Chevrons along the RDB (130-129.9)
14 Dikes along the LDB (134.3-128.6)
3.4 dikes/mile - 14\% notched

## Structure Changes:

Two dikes discounted in the 2002 report were present in the low water aerial photography. Two dikes (132.9 R, 132.8 R) were removed. The dike at RM 132.5 R was extended both, of the root and rootless. Two chevrons (130.0 R, 129.9 R) were constructed. One new dike constructed at RM 132.6 R in 2006; the survey suggested a scour hole had developed off the tip of the dike. Neither of the chevrons constructed along the RDB show evidence of scour hole development behind the structure.

Weirs: $\quad$ Establishment RDB (133) 4 Weirs
Fort Chartres LDB (131-130) 9 Weirs
Chutes: 2002:
0.69 miles/mile

Fort Chartres LDB (134.5-132.3) 1 closure
Establishment RDB (132.5-130.2) 5 closures
2006:
0.66 miles/mile

Fort Chartres LDB (134.3 - 132.3) 1 closure
Establishment RDB (132.5-130.2) 5 closures
Dredging: 11 cuts in the center of the channel at $\sim$ RM $130-$ RM 129 for a total of 1,767,341 CY

Priority: 2002:
2 Stars.

2011:
1 Star. - Recent GP for side channel enhancement at Establishment.

Conclusions: 2002:
Two side channels currently exist in the reach. Some possibilities exist in dike field 1. Many possibilities exist in dike field 2, especially within the bar in front of Establishment and Schmidts Islands. Modifications in dike field 3 may have the secondary benefit of reducing maintenance dredging in the crossing.

2011:
Field 1 - Medium. There are six dikes in this field, but they are shorter. This field encompasses Fort Chartres Chute.

Field 2 - Low. This field was the site of a recently completed HSR model study (2012) with a GP moving forward with construction. The recommended alternative would lead to the creation of a Side Channel Enhancement Dike (SCED) with the intended purpose of sending additional flow down the side channel, decreasing sedimentation in the channel promoting scour off downstream structures.
Field 3 - Medium. There are limited opportunities among the existing dikes; any dike work in this field would likely involve new construction. The opportunity for island creation exists among the existing dikes.

## REACH 10: STE. GENEVIEVE, 8.5 MILES (128-119.5)

Map: $\quad$ Appendix B, Figure 10
Characteristics: A gradual bend to the left then right between Miles 128 and 123, then straight to Mile 122, then a sharp bend to the left to Mile 120.

Slope: Water Surface: 0.54 feet $/$ mile
Width Bankline: 2038
Channel: 1063
Dikes: 2002:
34 Total Dikes ( 14 RDB \& 20 LDB)
4.0 dikes/mile - $9 \%$ notched

Dike Field 1: LDB continuous (125.5-119.5) 20 dikes
Dike Field 2: RDB continuous (125-122.5) 12 dikes
Dike Field 3: $\quad$ RDB (121.4-121.2) 2 trail dikes
2011:
36 Main Channel Structures
15 Dikes along RDB (124.9-121.2)
21 Dikes along the LDB (126.6-120.2)
4.2 dikes/mile - 17\% Notched

Structure Changes:
Two dikes ( $125.3 \mathrm{~L}, 121.45 \mathrm{R}$ ) discounted in the 2002 report were present in the low water aerial photography. Three dikes ( 130.2 R, 130.05 R, 129.9 R) were notched.

Weirs: $\quad$ Ste. Genevieve RDB (120.8-119.8) 10 Weirs
Chutes: 2002:
0.32 miles/mile

Moro LDB (122.7-120) 2 closures
2006:
No change.
Dredging: $\quad 14$ cuts for a total of $1,505,305 \mathrm{CY}$ :
10 cuts along the LDB and channel center at $\sim$ RM 126.5 - RM 125 for a total of 1,221,144 CY

4 cuts along the LDB and channel center at $\sim$ RM 122 - RM 121 for a total of 284,191
CY
Priority: 2002:
1 Star.
2011:
2 Stars. Opportunity for additional work with HSR model.
Conclusions: 2002:
The reach currently has one large side channel complex. The dike at the exit to Moro Chute is scheduled for notching. Areas between Miles 126 and 122 have been identified as habitat for the endangered Pallid Sturgeon. Therefore, modifications are not recommended until additional monitoring is completed. The greatest possibilities exist in dike fields $1 \& 2$, which secondarily may reduce the repetitive dredging in the crossing.

2011:
Field 1 - Medium. Opportunities exist with dikes at the lower end of the field. Additional work is possible with Moro Chute. This site has been proposed for studying with a model soon.
Field 2 - Medium. Opportunities exist in this field, but the dikes are shorter and the presence of pallid sturgeon is a concern that could lower the ability to work in the field. Field 3 - Low. This is a small field with no real opportunities.

## REACH 11: KASKASKIA, 10 MILES (119.5 - 109.5)

Map: $\quad$ Appendix B, Figure 11
Characteristics: Straight to Mile 117.5, then a severe 70-degree bend to the right to Mile 116.5, then straight to Mile 114, then a slight bend to the left to Mile 112, then straight to Mile 109.5. The confluence with the Kaskaskia River is located along the LDB at Mile 117.5L. The bluff line is located along the LDB.

Slope: Water Surface: 0.54 feet $/ \mathrm{mile}$
Width Bankline: 2210
Channel: 1220
Dikes: 2002:
53 Total Dikes (35 RDB \& 18 LDB)
5.3 dikes/mile - $6 \%$ notched

Dike Field 1: RDB continuous (119.5-116) 16 dikes
Dike Field 2: LDB continuous (116-111) 18 dikes
Dike Field 3: RDB continuous (114.5-112.5) 10 dikes
Dike Field 4: RDB continuous (111.5-110) 9 dikes
2011:
Three dikes (113.9 R, 113.5 R, 113.2 R) were extended.
Weirs: Kaskaskia LDB (117-116) 11 Weirs

Since 2002 - Kaskaskia LDB (117.2) 1 Weirs
Chutes: 2002:
0.20 miles/mile

Kaskaskia RDB (118-116) 1 closure
2006:
0.21 miles/mile

Beaver Island Complex (two channels) RDB (117.8 - 115.7) 5 closures
Dredging: $\quad 9$ cuts for a total of 2,210,101 CY:
2 cuts in the center of the channel at $\sim$ RM 117.5 for a total of 197,150 CY
2 cuts in the center of the channel at $\sim$ RM 115.5 for a total of $347,307 \mathrm{CY}$
5 cuts along the RDB at RM 113.4 - RM 112.4 for a total of 1,665,644 CY
Priority: 2002:
2 Stars.
2011:
3 Stars. - Many dikes in the reach with little modification.
Conclusions: 2002:
Environmental modifications have already been designed for the dikes at the lower end of Beaver Island. It is recommended that this work be completed and monitored before additional enhancements are designed. Other possibilities exist in all dike fields, especially with those dikes in front of Beaver Island, which may also provide a secondary benefit of reducing dredging between Miles 113 and 112. There are many dikes in this reach and only a few have been modified for environmental enhancement. The area also seems to provide important habitat for sturgeon.

2011:
Field 1 - High. Little opportunity exists at the upper end of the field, but there are opportunities associated with Kaskaskia Chute and Beaver Island.
Field 2 - Medium. Work was completed in this field within the last five years that needs further evaluation. Opportunities exist in the downstream section of the field, but pallid sturgeon presence is a concern.
Field 3 - Low. There are a number of dikes in this reach, but they are shorter and have accreted.
Field 4 - Medium. The channel is aligned with the beginning of the field, promoting beneficial development with structure modification.

## REACH 12: MILE 100 ISLANDS, 14.5 MILES (109.5 - 95)

Map: $\quad$ Appendix B, Figure 12
Characteristics: Straight to Mile 108, then a slight bend to the left then to the right between Miles 108 and 106, then straight to Mile 104, then another slight bend to the right then to the left between Miles 104 and 102, then straight to Mile 98.5, then a moderate 80 degree bend to the right to Mile 95. The LDB at the upstream end of the reach is located along the bluff line.

Slope: Water Surface: 0.55 feet/mile
Width Bankline: 3307

Dikes: 2002:
54 Total Dikes (43 RDB \& 11 LDB)
3.7 dikes/mile - 28\% notched

Dike Field 1: RDB continuous (108.7-102.5) 28 dikes
Dike Field 2: LDB (106.6-105.6) 4 dikes
Dike Field 3: LDB continuous (104-102) 7 dikes
Dike Field 4: RDB continuous (101-96) 15 dikes
2011:
72 Main Channel Structures
48 Dikes along RDB (108.7-96.2)
4 Chevrons along the RDB (104.4-103.4)
17 Total Dikes along the LDB (106.5-95.2)
3 Chevrons along the LDB (100.1-99.9)
5.0 dikes/mile - 25\% Notched

## Structure Changes

Seven chevrons have been constructed. Eleven dikes discounted in the 2002 report were present in the low water aerial photography. All of the chevrons constructed show evidence of scour hole development behind the structure. Two dikes (106.2 L, 105.9 L) have had sections disconnected from the dike root. Two rootless dike extensions (96.8 R, 96.6 R) were constructed. Three notches were constructed.

```
Weirs: 2002:
    None
    2011:
    Weir 103.2 L
Chutes: 2002:
    0 . 5 8 \text { miles/mile}
    Crains RDB (105 - 104) 0 closures
    Liberty LDB (103 - 100) }3\mathrm{ closures
    Strauser RDB (100-98.8) island complex 5 closures
    Jones RDB (98.2 - 95) }3\mathrm{ closures
    2006:
    0 . 6 1 \text { miles/mile}
    Crains RDB (105.7 - 104) }6\mathrm{ closures
    Liberty LDB (102.7 - 100) 3 closures
    Strauser RDB (100 - 98.8) dike and island complex
    Jones RDB (98.2 - 95) 2 closures
Dredging: }30\mathrm{ cuts for a total of 7,220,966 CY:
    14 cuts in the center of the channel at RM 104.1 - RM 101.8 for a total of 4,922,249 CY
    6 cuts in the center of the channel at RM 100.3 - RM 99 for a total of 601,448 CY
```

2 cuts in the center of the channel at $\sim$ RM 97.6 for a total of 273,570 CY
8 cut in the center of the channel at RM 96.8 - 95.8 for 1,423,699 CY
Priority: 2002:
1 Star.
2011:
1 Star.
Conclusions: 2002:
Most of the reach is very diverse with multiple islands and side channels. Approximately $28 \%$ of the existing dikes in this reach have already been notched. Three dikes on the LDB just downstream of the mouth of Mary's River (106.5 L) are scheduled for notching. Other possibilities exist in dike field 1 where diversity is the lowest of the 4 fields. A secondary benefit of these alterations may be a reduction of dredging in the crossings between Miles $103 \& 102$ and $100 \& 99.5$. Modifications may also be beneficial in the dike field 4, in front of Liberty Bar and Jones Towhead, which may also secondarily reduce dredging between Miles 97 \& 96 .

2011:
Field 1 - Medium. This field was the site of the Waters Landing HSR model study and GP. There has been significant accretion in this dike field. Opportunities for dike alteration exist associated with the Crains Island complex. It is recommended that the site be re-evaluated after the Waters Landing structures have their full effect. Field 2 - Medium. This is a short field that already contains notches in the field. However, the area is ripe for large island creation and improving Mary's Island river connectivity. Any additional dike work would likely be due to extension of the field upstream.
Field 3 - Medium. Limited opportunities exist in the field, but better separation of the sandbar at the downstream end of the field could be better separated from Rockwood Island. Dredging remains an issue in this field.
Field 4 - Medium. Work has been done in this field both with ARRA funding and as part of the Red Rock contract. The lower end of this field still presents an opportunity for enhancements. This field should be re-evaluated when all the effects of all recent work reaches equilibrium

This has been an incredibly active repetitive maintenance dredging location. Only one additional dike was notched in the period between reports, but chevrons and rootless dikes have been constructed between the side channel sections.

## REACH 13: RED ROCK TO TOWER ROCK, 15 MILES (95-80)

Map: Appendix B, Figure 13
Characteristics: Severe 60-degree bend to the left between Miles 95 and 93.5 where the river intersects the Missouri bluff line (Red Rock at Mile 94.5R) at the same angle, then relatively straight for 9 miles before a severe 80-degree bend to the right between Miles 85.5 and 83 where the river intersects the Illinois bluff line (Fountain Bluff at Mile 83.7L), then straight to the Devil's Bake Oven rock outcrop (Mile 81L), then a bend to the left to the Tower Rock (Mile 80R) outcrop.

Several bedrock controls are located this reach where 4 rock bluff lines severely intersect the river bankline and bottom. The river does not migrate away from a rock bluff line in this reach.

Slope: Water Surface: 0.54 feet/mile
Width Bankline: 2163
Channel: 1225

Dikes: 2002:
35 Total Dikes (14 RDB \& 21 LDB)
2.3 dikes/mile - 0\% notched

Dike Field 1: LDB Continuous (93-91.5) 6 dikes
Dike Field 2: RDB Continuous (91.5-90.5) 6 dikes
Dike Field 3: LDB Continuous (89.5-85) 15 dikes
Dike Field 4: RDB Continuous (86.5-85) 8 dikes

2011:
48 Main Channel Structures
18 Total Dikes along RDB (94.6-85.05)
1 Chevron along the RDB (90.4)
26 Total Dikes along the LDB (106.5-95.2)
3 Chevrons along the LDB (89.55-82)
3.2 dikes/mile - 8\% Notched

Structure Changes:
Five dikes discounted in the 2002 report were present in the low water aerial photography. Four new dikes (93.3L, 93.1L, 81.85, 81.65) were constructed in the reach. All dikes show evidence of scour occurring of the tips of the dikes. Four new chevrons ( $90.4 \mathrm{R}, 89.55 \mathrm{~L}, 89.15 \mathrm{~L}, 82.0 \mathrm{~L}$ ) were constructed in the reach. All four chevrons exhibited scour. Four notches were constructed. Rootless extensions were constructed off of three dikes (93.0 L, 89.3 L, 89.0 L). Two dikes (89.3 L, 89.0 L) were extended.

Weirs: $\quad$ Red Rock RDB (95-93.7) 9 Weirs
Fountain Bluff LDB (84-83) 10 Weirs
Since 2002 - Fountain Bluff RDB (82.5-82.4) 2 Weirs
Chutes: 2002:
0.15 miles/mile

Owl Creek Bar RDB (84.8-82.5) 17 Hard Points along bankline
2006:
No change.
Dredging: $\quad 21$ cuts for a total of $1,870,202$ CY:
3 cuts in the center of the channel at RM 99.8 - RM 94.3 for a total of 242,236 CY
4 cuts in the center of the channel at RM 93.4 - RM 92 for a total of 480,748 CY
4 cuts in the center of the channel at RM 82.6-81.2 for a total of 273,570 CY
10 cuts in the center of the channel at $\sim$ RM 80.3for $908,377 \mathrm{CY}$

Priority: 2002:
5 Stars.
2011:
4 Stars. Dike construction, chevron construction, and notching have occurred and construction warrants further monitoring.

Conclusions: 2002:
This is a very unique reach with numerous bedrock bluffs and controls but without a significant backwater or side channel. The two weir fields and the hard points at Owl Creek Bar provide the only diversity. This reach has been repeatedly identified as a reach that requires biological enhancement. Good possibilities exist between miles 93 and 85 where many dikes exist but only very minimal dredging occurs and the RDB is firmly against the rock bluff line. New environmental structures could be placed between miles 82 and 81 where the banks widen. These structures may have a secondary benefit of reducing the repetitive dredging in this area.

2011:
Field 1 - Low. A number of these dikes were extended and notched in 2010 and 2011. Some opportunity still remains. It is recommended that the recent work be monitored and revisited at a future time.
Field 2 - Medium. Work was completed in this field under the Biological Opinion program. Evaluation of this work is ongoing.
Field 3 - Medium. Work was completed in this field under the Biological Opinion program. Evaluation of this work is ongoing.
Field 4 - Medium. Little opportunity in this field among the existing dikes, but extension of the field to isolate the Owl Creek sandbar from the mainland would have significant benefit.

This remains a reach with potential. This reach continues to require repetitive maintenance dredging, but the LDB between RM $90-85$ remains a possibility for alteration. The Owl Creek side channel remains mostly closed, and may be an opportunity for further rehabilitation.

## REACH 14: BIG MUDDY, 9 MILES (80 - 71)

Map: $\quad$ Appendix B, Figure 14
Characteristics: A slight bend to the right between Miles 80 and 78, then a gradual bend to the left to Mile 76.5 ,then straight to Mile 73.5, then a another slight bend to the left to Mile 72.5, then straight to Mile 71. The bluff line is located along the RDB.
The confluence with the Big Muddy River is located along the LDB at Mile 75.6L
Slope: Water Surface: 0.61 feet/mile
Width Bankline: 2525
Channel: 1050
Dikes: 2002:
35 Total Dikes (8 RDB \& 27 LDB)
3.9 dikes/mile - 11\% notched

Dike Field 1: LDB (79.3 - 79) 2 small dikes
Dike Field 2: LDB continuous (78.2-71) 25 dikes
Dike Field 3: RDB sporadic (79.5-71) 8 dikes, scattered throughout reach
2011:
38 Main Channel Structures
7 Total Dikes along RDB (75.5-71)
31 Total Dikes along the LDB (79.5-71)
4.2 dikes/mile - $16 \%$ Notched

Structure Changes:
Four dikes ( $79.5 \mathrm{~L}, 75.3 \mathrm{~L}, 74.1 \mathrm{~L}, 71.3 \mathrm{R}$ ) discounted in the 2002 report were present in the low water aerial photography. One dike ( 71.0 R ) that was counted in the 2002 report was considered to be in the next reach. Two dikes ( $75.5 \mathrm{~L}, 75.2 \mathrm{~L}$ ) were notched. Three rootless extensions ( $72.4 \mathrm{~L}, 72.1 \mathrm{~L}, 71.9 \mathrm{~L}$ ) were constructed.

Weirs: None
Chutes: 2002:
0.48 miles/mile

Cottonwood RDB (79.5-77.5) 0 closures
Crawford LDB (73.8-71.5) 0 closures
2006:
0.47 miles/mile

Cottonwood RDB (79.3-77.5) 0 closures
Crawford LDB (73.8-71.4) 0 closures
Dredging: 25 cuts for a total of $2,241,165 \mathrm{CY}$ :
17 cuts in the center of the channel at RM 79.7 - RM 74.7 for a total of $1,483,978$ CY 8 cuts in the center of the channel at RM 73.4 - RM 71.7 for a total of 757,187 CY

Priority: 2002:
2 Stars.
2011:
1 Star. - Additional notching has been done.
Conclusions: 2002:
Two side channels currently exist in the reach. The Cottonwood Chute may be the deepest and most functional side channel on the Middle Mississippi River. Two dikes on the LDB just downstream of the mouth of the Big Muddy River have recently been notched. The greatest possibilities for alterations exist mainly within dike field 2.

2011:
Field 1 - Low. This is a short field with only three short dikes.
Field 2 - High. Recent work has been done, with additional work planned around Crawford Towhead in FY13. Further work and opportunities for habitat enhancement exist below Big Muddy Island and near Crawford Towhead.

Field 3 - Low. While this is a long field, it contains only a few dikes with limited opportunities.

## REACH 15: TRAIL OF TEARS, 8.5 MILES (71 - 62.5)

Map: $\quad$ Appendix B, Figure 15
Characteristics: A slight bend to the left to Mile 69, then straight to Mile 66, then a slight bend to the right to Mile 64, then straight to Mile 62.5. The bluff line is located along the RDB.

| Slope: | Water Surface: | 0.59 |
| :--- | :--- | ---: |
| Width | Bankline: | 2300 |
|  | Channel: | 1411 |

Dikes: 2002:
53 Total Dikes (22 RDB \& 31 LDB)
6.2 dikes/mile - $25 \%$ notched

Dike Field 1: $\quad$ LDB continuous ( $71-62.5$ ) 31 dikes, stubby near D/S end
Dike Field 2: $\quad$ RDB continuous $(71-69) 5$ dikes
Dike Field 3: RDB continuous (67.5-62.5) 17 dikes
2011:
55 Main Channel Structures
23 Dikes along RDB (70.7-62.5)
32 Dikes along the LDB (70.6-62.5)
6.5 dikes/mile - $24 \%$ Notched

Structure Changes:
One dike ( 69.8 L ) discounted in the 2002 report were present in the low water aerial photography. One dike ( 71.0 R ) was included in this reach that had been included in another reach in the 2002 report.

Weirs: $\quad$ Hanging Dog LDB (70.5-70) 5 Weirs
Chutes: 2002:
None - 0.0 miles/mile
2006:
0.04 miles/mile

Vancill Towhead LDB (67.7-67.4)
Dredging: 20 cuts for a total of 2,929,416 CY:
6 cuts in the center of the channel at RM 71.2 - RM 69.0 for a total of 655,279 CY
10 cuts in the center of the channel at RM 68.0 - RM 67.1 for a total of 1,896,350 CY
3 cuts in the center of the channel at RM $66.2-65.2$ for a total of $305,559 \mathrm{CY}$
1 cuts in the center of the channel at $\sim$ RM 64.0 for 72,228 CY
Priority: 2002:
5 Stars.

2011:
5 Stars.
Conclusions: 2002:
This is a relatively straight reach without a side channel. Possibilities exist within all dike fields. Modifications between miles 68 and 67 may be able to establish a side channel where the banklines widen near the bar at Vancill Towhead. This may also have a secondary benefit of improving depths in the navigation channel thereby reducing dredging. This area provides an excellent opportunity that should not be overlooked, but is at the current time the Biological Monitoring area for the NESP project at Herculaneum (RM 68.5 - 64.5).

2011:
Field 1 - High. This field is being modeled as part of the Vancill Towhead HSR model. The possibility for island creation exists in this field.
Field 2 - Medium. This field is being modeled as part of the Vancill Towhead HSR model.
Field 3 - High. There are opportunities for island creation through dike modification and placement, though no construction is planned at this time.

This remains an active dredging area with no construction efforts outside of weir restoration. A currently ongoing (2012) HSR model study is examining alternatives to alleviate maintenance dredging and presents an opportunity for habitat-beneficial construction.

## REACH 16: SCHENIMANN/PICAYUNE, 8.5 MILES (62.5-54)

Map: $\quad$ Appendix B, Figure 16
Characteristics: Straight to Mile 61.5, then a slight bend to the right to Mile 60.5, then straight to Mile 59, then a 70 degree bend to the right to Mile 57, then straight to Mile 55.5, then a 40 degree bend to the left caused by the Cape Rock outcrop (Mile 54R). The only bluff line is located at the end of the reach at Cape Rock.

Slope: Water Surface: 0.57 feet/mile
Width Bankline: 5700
Channel: 1050
Dikes: $\quad 46$ Total Dikes ( 23 RDB \& 23 LDB)
5.4 dikes/mile - 9\% notched

Dike Field 1: LDB continuous (62.5-60.5) 11 dikes
Dike Field 2: RDB continuous (62.5-57) 19 dikes, bordering Schenimann Chute
Dike Field 3: LDB sporadic ( $59-54.5$ ) 12 dikes, mostly stub
Dike Field 4: RDB continuous (56.5-55.8) 4 dikes
2011:
49 Main Channel Structures
25 Total Dikes along RDB (62.2-55.8)

24 Total Dikes along the LDB (62.2-54.8)
5.8 dikes/mile - 12\% Notched

## Structure Changes:

Three dikes ( 60.6 R, 60.2R, 56.3 L ) discounted in the 2002 report were present in the low water aerial photography. Three ( 62.2 R, $55.2 \mathrm{~L}, 54.8 \mathrm{~L}$ ) notches were constructed.

Weirs: $\quad$ Picayune LDB (58-56) 14 Weirs
Upper Cape Rock RDB (55-54.5) 4 Weirs
Chutes: 2002:
1.38 miles/mile

Schenimann RDB (62.5-57) 5 closures
Picayune LDB (61-54.8) 2 closures
2006:
1.33 miles/mile

Schenimann RDB (62.4-57) 9 closures
Picayune LDB (60.7-54.8) 3 closures
Dredging: $\quad 7$ cuts for a total of $2,558,436 \mathrm{CY}$ :
4 cuts in the center of the channel at RM 59.2 - RM 57.7 for a total of 505,523 CY
3 cuts in the center of the channel at $\sim$ RM 55.0 for a total of $363,903 \mathrm{CY}$
Priority: 2002:
2 Stars.

2011:
2 Stars.
Conclusions: 2002:
Two lengthy side channels currently exist in this reach. Environmental enhancements are scheduled to be constructed in Schenimann Chute - see the Schenimann Chute Micro Model Study Report M15. Possibilities mostly exist in dike field 1, 2, and 4. Dike field 3 consists of mainly stub dikes. Modifications should be made to the structures located at the lower end of Schenimann Island to maintain the small backwater chutes that exist here. These modifications could also have a secondary benefit of reducing the repetitive dredging that occurs in the channel crossing adjacent to the backwater areas.

2011:
Field 1 - Medium. Localized opportunities exist for dike-specific modifications. The bar adjacent to the mouth of Picayune Chute, however, has great opportunity for better separation and access to the chute.
Field 2 - High. Further work is on hold as effects of recent ARRA work are still being realized with monitoring planned. Long-term, this site presents a great opportunity for dike habitat enhancement associated with Schenimann Chute habitat complex development.
Field 3 - Low. This field contains a number of shorter dikes.
Field 4 - Low. This is a short field with only four short dikes.

Additional notching has been done in this reach since 2002. Dredging has occurred in the past, but not in 2010 or 2011, not to the extent of other reaches, and mainly in channel bends.

## REACH 17: CAPE GIRARDEAU, 8 MILES (54-46)

Map: Appendix B, Figure 17
Characteristics: Straight to Mile 53, then a 40-degree bend to the left to Mile 52, then straight along the RDB bluff line and the City of Cape to Mile 50, then a 100-degree bend to the left to Mile 48.5, then straight with another bluff line along the RDB to Mile 46.5, then the beginning of a tortuous bend at Grays Point. The bluff line is adjacent to the RDB from the upper end of the reach at Cape Rock through the City of Cape Girardeau. Another bluff line resumes on the RDB after the 100 -degree bend.

Slope: Water Surface: 0.58 feet/mile
Width Bankline: 3244
Channel: 1056
Dikes: 2002:
17 Total Dikes (3 RDB \& 14 LDB)
2.1 dikes/mile - $0 \%$ notched

Dike Field 1: LDB continuous (53-50) 11 dikes
Dike Field 2: $\quad$ RDB $(48-47) 3$ dikes
Dike Field 3: LDB (47.5-47) 3 dikes
2011:
19 Main Channel Structures
3 Dikes along RDB (47.9-47.2)
16 Dikes along the LDB (53-47)
2.4 dikes/mile - 11\% Notched

Structure Changes:
Two dikes (49.7 L, 48.6 L) discounted in the 2002 report were present in the low water aerial photography. Two notches ( $51.0 \mathrm{~L}, 50.6 \mathrm{~L}$ ) were constructed.

Weirs: $\quad$ Lower Cape Rock RDB (54) 4 Weirs at the Cape Rock protrusion Cape Bend RDB (49.5-48.2) 13 Weirs

Chutes: 2002:
0.31 miles/mile

Marquette LDB (51-48.5) 4 closures
2006:
0.41 miles/mile

Marquette LDB (51-47.7) 4 closures
Dredging: 18 cuts for a total of $1,152,438 \mathrm{CY}$ :
4 cuts in the center of the channel at RM 53.8 - RM 53.1 for a total of 232,661 CY

2 cuts in the center of the channel at RM 50.2 - RM 49.3 for a total of 268,877 CY 9 cuts in the RDB at RM $48.5-47.9$ for a total of 436,159 CY
3 cuts in the center of the channel at $\sim$ RM 47.1 for 214,741 CY
Priority: 2002:
3 Stars.
2011:
2 Stars. - Notching has taken place.
Conclusions: 2002:
One large side channel currently exists in the reach and the area may provide important habitat for sturgeon. Although few dikes are available, there are none that are notched. However, modifications to the four dikes near the upstream of Marquette Chute have recently been constructed. These dikes were raised and lengthened to reduce dredging. Two of these dikes will be further modified with environmental notches funded under O\&M. Possibilities exist in all dike fields but especially in field 1 where more structures are located. Many alternatives have already been evaluated for Marquette Chute - see Marquette Chute Micro Model Study Report M3.

2011:
Field 1 - High. Opportunities exist in the lower end of the field associated with Marquette Chute. The site has been identified by the Corps's environmental partners as an area of interest.
Field 2 - Low. This is a short field with only three short dikes and fleeting in the vicinity. Field 3 - Medium. Opportunities exist associated with the exit of Marquette Chute.

The only construction activity in this reach has been dike notching. Dredging is scattered in this reach with the largest portion being at SEMO Port.

## REACH 18: THEBES, 11MILES ( 46 - 35 )

Map: $\quad$ Appendix B, Figure 18
Characteristics: Extremely tortuous 110-degree bend to the right at Gray's Point (Mile 46R) at the beginning of Thebes Gap or the Grand Chain, then straight to Mile 44.5, then a 40 degree bend to the left to Mile 43, then relatively straight to Mile 37, then a slight bend to the left to Mile 36, then straight to Mile 35. The Thebes Gap is a 6 -mile long bedrock controlled geologic feature with bluff lines located along both riverbanks from Gray's Point to the head of Burnham Island and Sante Fe Chute at Mile 40. Water surface slopes are almost double the average of 0.5 foot/mile in this reach. Downstream of this structure is an alluvial valley without rock outcroppings.

Slope: Water Surface: 0.57 feet/mile
Width Bankline: 3780
Channel: 1160
Dikes: $\quad 45$ Total Dikes ( 23 RDB \& 22 LDB)
4.1 dikes/mile - $2 \%$ notched

Dike Field 1: $\quad$ RDB continuous (44.5-43.5) 4 dikes
Dike Field 2: LDB continuous (43-39.5) 9 dikes
Dike Field 3: RDB continuous (42-37.5) 19 dikes
Dike Field 4: LDB continuous along Burnham Island (38.5-35) 13 dikes

2011:
54 Main Channel Structures
27 Total Dikes along RDB (44.9-35)
23 Total Dikes along the LDB (45.9-35)
4 Chevrons along the LDB (36.7-35.9)
49.9 dikes/mile - 4\% Notched

Structure Changes
Three dikes (40.6 R, 37.7 L, 35.7 L) discounted in the 2002 report were present in the low water aerial photography. Three new dikes ( $44.9 \mathrm{R}, 44.7 \mathrm{R}, 35.1 \mathrm{R}$ ) and four new chevrons ( $36.7 \mathrm{~L}, 36.5 \mathrm{~L}, 36.2 \mathrm{~L}, 35.9 \mathrm{~L}$ ) were constructed. Three of the four chevrons exhibit scour behind the structure in the 2010; the area behind the fourth structure was not surveyed due to the presence of rootless trail dikes. One dike (35.0L) that was included in this reach in the 2002 report was included in another reach. One dike ( 39.6 L ) was notched.

Weirs: $\quad$ Since 2002 - LDB (39.6) 1 Weir
Chutes: 2002:
0.64 miles/mile

Thebes Chute LDB (42-39.5)
Sante Fe LDB (39.5-35) 1 closure \& 7 hard points
2006:
0.63 miles/mile

Rock Island LDB (45.8-45.5)
Thebes Chute LDB (41.7-39.5)
Santa Fe LDB (39.5-35.1)
Dredging: $\quad 27$ cuts for a total of 3,076,552 CY:
9 cuts in the center of the channel at RM 46.2 - RM 43.9 for a total of 645,850 CY
14 cuts in the center of the channel at RM 42.2 - RM 38.1 for a total of 1,863,680 CY
4 cuts in the center of the channel at RM 36.6 - RM 35.1 for a total of 567,022 CY

Priority: 2002:
4 Stars.

2011:
4 Stars.

Conclusions: 2002:
Several dikes in this reach are scheduled for modifications to reduce dredging. The small and relatively unnoticed Thebes Chute could be enhanced with further modifications. Seven hard points were constructed in Sante Fe Chute in 1997. - See Sante Fe Micro Model Study Report M1. Possibilities may exist in all dike fields although intended
results may not be met in the areas of rock outcrops. The rock outcrops may control most of the modifications to the reach.

2011:
Field 1 - Low. This is a short field with dike-specific opportunities.
Field 2 - High. Offset dikes are currently planned for construction in this field. Potential for habitat enhance,ent remains associated with Santa Fe chute.
Field 3 - Low. The construction of offset dikes is planned for the dikes from RM 39.4 to RM 38.6 in FY12. The majority of the remaining dikes in the field are short and limit the opportunity for enhancement.
Field 4 - Low. Recent work was completed in this field, including the construction of three chevrons and the introduction of the runway chevron.

Numerous structures in this reach have undergone restoration but little notching (possibly due to the rock mentioned previously. Dredging remains an issue, especially near the entrance to Santa Fe Chute.

## REACH 19: PRICES, 6 MILES (35-29)

Map: $\quad$ Appendix B, Figure 19
Characteristics: A long bend to the right of 50 degrees to Mile 32.5, then straight to Mile 31, then a sharp 80-degree bend to the left to Mile 30, then straight to Mile 29.

Slope: Water Surface: 0.55 feet/mile
Width Bankline: 2671
Channel: 1029

Dikes: 2002:
15 Total Dikes (7 RDB \& 8 LDB)
2.5 dikes/mile - $0 \%$ notched

Dike Field 1: RDB sporadic $(35-32) 7$ dikes
Dike Field 2: LDB continuous (32-31) 8 dikes, mainly D/S angled
2011:
19 Main Channel Structures
6 Dikes along RDB (34.8-32)
3 Chevrons along RDB (32.8-32.4)
10 Dikes along the LDB (34.2-31.1)
3.2 dikes/mile - 0\% Notched

Structure Changes:
Two dikes (34.1 L, 32.2 L) discounted in the 2002 report were present in the low water aerial photography. One dike ( 35.1 R ) was counted in this reach in 2002 despite being outside the reach. Three chevrons ( $32.8 \mathrm{R}, 32.6 \mathrm{R}, 32.4 \mathrm{R}$ ) were constructed. All three chevrons show evidence of downstream scour hole formation.

Weirs: $\quad$ Prices RDB (30.5-29.5) 9 Weirs

Chutes: 2002:
0.45 miles/mile

Billings RDB (34-33.3) 0 closures
Bumgard Bar LDB (31-29) 5 hard points
2006:
0.42 miles/mile

Billings RDB (34-33.3) 0 closures
Bumgard Bar LDB (31.1-29.3) 5 hard points

Dredging: $\quad 16$ cuts for a total of $1,741,942 \mathrm{CY}$ :
3 cuts in the center of the channel at RM 34.5 - RM 33.4 for a total of 544,689 CY
7 cuts in the center of the channel at RM 32.9 - RM 31.7 for a total of 706,161 CY
6 cuts in the center of the channel at RM 31.7 - RM 30.6 for a total of 491,092 CY
Priority: 2002:
2 Stars.
2011:
2 Stars.
Conclusions: 2002:
Two side channels currently exist in the reach. Although currently there are not any notched dikes, there are only a small number of dikes that are available for modifications. Possibilities exist in both dike fields. However, the alterations could have a secondary benefit of reducing repetitive dredging in the crossing between Miles 31.5 and 30.5.

2011:
Field 1 - Medium. Three chevrons were constructed in the lower end of this field, but opportunities remain in the upper end of this field through construction and enhancement. Field 2 - Medium. This area is currently being studied with the Bumgard Island HSR model.

No notches have been constructed, but three chevrons have been built that show evidence of downstream scour. Dredging remains an issue between RM 33 - 30.5.

## REACH 20: DOGTOOTH, 9 MILES (29 - 20)

Map: Appendix B, Figure 20
Characteristics: Straight to Mile 26.5, then a slight bend to the right to Mile 25.5, then straight to Mile 24.5, then a severe 180-degree bend to the left to Mile 20.

Slope: Water Surface: 0.61 feet/mile
Width Bankline: 3350
Channel: 938

Dikes: 2002:
27 Total Dikes (10 RDB \& 17 LDB)
3.0 dikes/mile - 4\% notched

Dike Field 1: LDB (28-27) 4 dikes
Dike Field 2: RDB continuous (27.6-25) 10 dikes
Dike Field 3: LDB continuous (25.5-24) 10 dikes, all D/S angled
Dike Field 4: LDB (21.6-20.5) 3 dikes
2011:
32 Total Structures
12 Total Dikes along RDB (27.6-24.6)
19 Total Dikes along the LDB ( 28 - 20.5)
1 Chevron along the LDB (21.8)
3.6 dikes/mile - 3\% Notched

Structure Changes:
One dike (24.6 R) discounted in the 2002 report was present in the low water aerial photography. One dike ( 23.3 R) not identified in the 2002 report was in the low water aerial photography. Two new dikes ( $22.1 \mathrm{~L}, 21.4 \mathrm{~L}$ ) were constructed. One chevron (21.8) was constructed. The three new structures were constructed in 2011 and have yet to be re-surveyed.

Weirs: $\quad$ Dogtooth RDB (24-22.5) 13 Weirs
Chutes: 2002:
0.49 miles/mile

Buffalo RDB (26.2-24.8) 1 closure
Browns LDB (24.5-21.5) 2 closures
2006:
0.48 miles/mile

Buffalo RDB (26.1-24.7) 1 closure
Browns LDB (24.8 - 21.9) 2 closures
Dredging: 18 cuts for a total of $4,683,743$ CY:
6 cuts in the center of the channel at RM 11.7 - RM 10.9 for a total of 1,706,545 CY
5 cuts along the RDB at RM 25.0 - RM 23.9 for a total of 1,366,953 CY
6 cuts in the center of the channel at RM 22.5 - RM 21.3 for a total of 1,483,292 CY
1 cut in the center of the channel at $\sim$ RM 20.5 for $126,593 \mathrm{CY}$
Priority: 2002:
2 Stars.
2011:
2 Stars.
Conclusions: 2002:
Few dikes currently contain notches; however, many possibilities exist for environmental enhancement in all dike fields. The alterations could have a secondary benefit of reducing repetitive dredging in the crossing between Miles 25 and 24.

2011:
Field 1 - Medium. This is a short field with four short dikes. This field is just downstream of a proposed flexible pipe location, and the field could be extended to support the use of the flexible pipe.
Field 2 - High. Opportunities exist for habitat complex development associated with Buffalo Chute and Browns Bar. Work in this field could affect the Buffalo Chute project. Field 3 - Low. There are opportunities in this field associated with Browns Bar, but the area is considered sensitive and any work in the field would need to be modeled.
Field 4 - Low. Recent work was completed in this field.

The situation remains largely the same. This reach remains a considerable dredging reach that has resisted solutions despite a model study being done.

## REACH 21: THOMPSON, 8 MILES (20-12)

Map: $\quad$ Appendix B, Figure 21
Characteristics: Straight to Mile 18, then a severe 180-degree bend to Mile 12.
Slope: Water Surface: 0.32 feet/mile
Width Bankline: 2422
Channel: 1078

Dikes: 2002:
25 Total Dikes (20 RDB \& 5 LDB)
3.1 dikes/mile - 20\% notched

Dike Field 1: $\quad$ RDB continuous (19.7-16.7) 12 dikes, many D/S angled
Dike Field 2: RDB continuous (15.5-13.5) 8 dikes
Dike Field 3: LDB continuous (13.7-13) 5 dikes, most with trails

2011:
30 Main Channel Structures
23 Dikes along the RDB (19.7-13.4)
7 Dikes along LDB (16.9-13.1)
3.8 dikes/mile - 17\% Notched

Structure Changes:
Two dikes (16.0 R, 14.3 R) discounted in the 2002 report were present in the low water aerial photography. Three dikes ( $16.9 \mathrm{~L}, 16.8 \mathrm{~L}, 13.4 \mathrm{R}$ ) not identified in the 2002 report were present in the low water aerial photography. Two of the dikes appeared to be partially removed for the installation of a weir field but are still evident; the third previously unidentified structure was a pile dike present in 1950s hydro books.

Weirs: $\quad$ Scudders LDB (17.3-16.7) 10 Weirs

| Chutes: | 2002: |
| :---: | :---: |
|  | 0.71 miles/mile |
|  | Thompson RDB (19-15.8) 0 closures (disconnected from U/S end) |
|  | Sister RDB (14.5-12) 2 closures |
|  | 2006: |
|  | 0.68 miles/mile |
|  | Thompson RDB (18.7-15.8) 0 closures (disconnected from U/S end) |
|  | Sister RDB (14.4-11.9) 3 closures |
| Dredging: | 9 cuts for a total of 1,855,230 CY: |
|  | 7 cuts along the LDB at RM 16.2 - RM 14.7 for a total of 1,496,092 CY |
|  | 2 cuts in the center of the channel at RM 14.1-RM 13.3 for a total of 359,138 CY |
| Priority: | 2002: |
|  | 1 Star. |
|  | 2011: |
|  | 1 Star. |

Conclusions: 2002:
Two side channels currently exist in this reach and $20 \%$ of the dikes are already notched. Opportunities for environmental enhancements exist in all dike fields. A secondary benefit of environmental alterations may be a reduction of repetitive dredging along the LDB throughout much of the reach, especially between Miles 16 and 15 .

2011:
Field 1 - Medium. This field was recently modeled as part of the Grand Lake Towhead HSR model study. Options were explored in this field with the goal of downstream potential effects, but model results were inconclusive.
Field 2 - Medium. Opportunities exist in this field in conjunction with Sister Chute and Island \#28, but the Grand Lake Towhead HSR model study was unable to find a solution to the ongoing dredging issues.
Field 3 - Low. This is a short field with only dike-specific modifications possible.

## REACH 22: CAIRO, 12 MILES (12 - 0)

Map: Appendix B, Figure 22
Characteristics: Straight to Mile 10, then a slight bend to the left to Mile 8, then a bend to the right to Mile 6, then straight to Mile 5, then a sharp 110 degree bend to the left to Mile 2, then straight to Mile 0 and the Ohio River confluence.

Slope: Water Surface: 0.29 feet $/$ mile
Width Bankline: 3636
Channel: 1045
Dikes: 2002:
33 Total Dikes (10 RDB \& 23 LDB)
2.8 dikes/mile - 3\% notched

Dike Field 1: LDB continuous (12-9.8) 11 dikes
Dike Field 2: RDB continuous (10.2-9.5) 7 hard points (stubs)
Dike Field 3: LDB continuous (8.7-6.5) 7 dikes
Dike Field 4: LDB continuous ( $5.5-4$ ) 5 dikes
Dike Field 5: RDB continuous (1.5-0.8) 3 dikes
2011:
42 Main Channel Structures
13 Dikes along RDB (10.1-0.1)
29 Dikes along the LDB (11.9 - 4)
3.5 dikes/mile - 12\% Notched

Structure changes:
Two dikes ( $7.5 \mathrm{~L}, 6.1 \mathrm{~L}$ ) discounted in the 2002 report were present in the low water aerial photography. Four dikes ( 6.7 R, 0.6 R, 0.3 R, 0.1 R) not identified in the 2002 report were present in the low water aerial photography. One dike ( 9.5 R ) present in the 2002 report was not visible in the 2006 aerial photography. Four dikes have been constructed since the last survey ( $9.4 \mathrm{R}, 9.2 \mathrm{R}, 8.3 \mathrm{~L}$, and the W-Dike at 4.0 L ). Four notches have been constructed.

| Weirs: | Eliza Point LDB (6.7-5.7) 10 Weirs Greenfield RDB (4.2-3) 9 Weirs Bird's Point RDB (2) 3 Weirs |
| :---: | :---: |
| Chutes: | $\begin{aligned} & \text { 2002: } \\ & 0.52 \text { miles/mile } \\ & \text { Boston LDB (10.2 - 7.5) } 2 \text { closures } \\ & \text { Angelo LDB (5 - 1.5) } 2 \text { closures } \end{aligned}$ |
|  | 2006: <br> 0.49 miles/mile <br> Boston LDB (10.2-7.7) 2 closures <br> Angelo LDB (5-1.6) 2 closures |
| Dredging: | 34 cuts for a total of $3,657,364 \mathrm{CY}$ : <br> 2 cuts in the center of the channel at RM 11.7 - RM 10.9 for a total of $397,639 \mathrm{CY}$ 4 cuts in the center of the channel at RM 9.7 - RM 8.4 for a total of 627,546 CY 4 cuts in the center of the channel at RM 7.3 - RM 6.4 for a total of 273,652 CY 1 cut in the center of the channel at $\sim$ RM 4.5 for 137,902 CY 5 cuts in the center of the channel at RM 2.9 - RM 2.2 for a total of $506,285 \mathrm{CY}$ 18 cuts in the center of the channel at RM 1.3 - RM 0 for a total of $1,714,340$ CY |
| Priority: | $\begin{aligned} & \text { 2002: } \\ & 3 \text { Stars. } \end{aligned}$ |

2011:
2 Stars. - Additional notching has taken place.

2002:
Possibilities for environmental enhancement exist in all dike fields. These alterations may have the secondary benefit of reducing repetitive dredging along the RDB between Miles $9 \& 8$ and $5 \& 4$ as well as to those areas between Miles $3 \& 0$.

2011:
Field 1 - Medium. Dike modifications were included as part of the approved Bi-Op model outcome for Boston Chute.
Field 2 - Low. This is a short field containing six short dikes.
Field 3 - Low. This field contains a number of shorter dikes and weirs. Modifications have already been undertaken in the upstream portion of the field.
Field 4 - Low. ARRA funding in this field supported the construction of a W-dike, multiple roundpoint structures, and dike notching. The area continues to be monitored. Field 5 - Low. This is a sensitive area for the navigation industry given the proximity of the bridge and difficult currents in the area.

## STRUCTURE DESCRIPTIONS

The following descriptions outline the structures currently employed by St. Louis District staff to attempt to meet the navigational and environmental components of the Corps's mission on the Mississippi.


Bendway Weirs - The Bendway Weir is a low level, totally submerged rock structure that is positioned from the outside bankline of the riverbend and angled upstream toward the flow. These underwater structures extend directly into the navigation channel underneath passing tows. Their unique position and alignment alter the river's spiraling, secondary currents in a manner which shifts the currents away from the outside bankline. This controls excessive channel deepening and reduces adjacent riverbank erosion on the outside bendway. Because excessive river depths are controlled, the opposite side of the riverbank is widened naturally. This results in a wider and safer navigation channel through the bend without the need for periodic maintenance dredging. The Bendway Weir also eliminates the need for dikes to be constructed on the inside of the bendway, protecting bend interior sandbar habitat. There had been concern that bendway weir construction was leading to increased bend-interior slopes; analysis of pre- to post-construction data found that slope changes were largely within the expected natural deviation ${ }^{1}$.

Bullnoses - Bullnoses redirect flows around islands protecting the islands from erosion. Without the rounded upstream rock structures, island heads can be exposed to high-velocity flows that hit head-on and mobilize sediment, eroding an island away. The bullnose locks

[^0]in the island's upstream geometry, rendering the island, and the aquatic and terrestrial habitat it forms, largely permanent.


Chevrons - Chevrons are "U"- or "V"-shaped rock structures with their apexes oriented upstream that divide flow smoothly so that a portion of the flow can be redirected without a significant undesired scour area forming. Dividing the flow in this manner can increase energy and decrease sedimentation in both side channels and the main channel. Besides redirecting flow along the front of the chevron, chevrons are designed with intent of periodic overtopping of the apex occurring. This overtopping results in the formation of a plunge pool within the chevron. The lower-velocity flow exiting the plunge pool can no longer maintain its sediment load and deposits sediment downstream of the chevron. This deposition can lead to the development of ephemeral or permanent islands downstream of chevrons. The bathymetric diversity presented by a plunge pool and downstream depositional area have been found to be favorable habitat for a variety of fish species. In the case of two or more chevrons, deposition behind the chevrons and side channel depth both increased with the number of chevrons. Use of multiple chevrons in a field can be used to either maintain a split flow situation or direct a split flow to a particular location (such as an area prone to a lower energy level). The
disadvantage to the construction of chevrons is that they obstruct far less flow than a typical dike of equivalent length. Chevrons can be constructed with rootless trails extending the effective length of the chevron legs with regards to splitting flow while allowing for some flow behind the chevron. They can also be constructed with notches, with the intent of decreasing the depth of the plunge pool; these effects are still being studied. A third option for chevron construction is the shortening of one leg and the extension of the other. This J-shape can be used to further maintain a split flow.

Hard Points - Hard points are very short rock dikes that are used to stabilize side channel river banks. The structures extend from the bank into the side channel and do not cause a significant buildup of sediment. Their contribution to habitat
 improvement is the creation of scour holes behind the hard points. These plunge holes attract fish that flourish in this environment. Effective hardpoint placement
 requires a relatively active side channel with little ongoing sedimentation.

J-Hooks - J-Hook Rock Vanes are structures designed to redirect velocity distribution and high velocity gradient in the near-bank region, stabilize stream-banks, dissipate energy in deep, wide, and long pools created below the structure, and create holding cover for fish and spawning habitat in the tail-out
of the structure. The basic function of the structure utilizes the principle that water will flow over immoveable objects at right angles ( $90^{\circ}$ angles). The device is constructed of large stone that is tied into the streambank. The stone is trenched into two rows at an upstream angle of $20^{\circ}$ to $30^{\circ}$ at a distance of $1 / 3$ stream width. The stone is then formed into a hook shape to cover a distance of $1 / 3$ stream width. The downstream row of rock is trenched into the stream bottom so that the top of the rock is approximately level with the stream bottom. The second row of rock is then placed just upstream of that row of rock slightly overlapping it so that as the water flows over the top of the upstream line of rock it will flow onto the downstream line of rock. This creates a stable surface on which the energy of the stream can be dissipated without completely scouring the stream bottom. As the stream dissipates its energy, it will scour the stream bottom slightly, creating a small scour pool immediately downstream of the device that serves as a source of aquatic habitat.

L-Dike - L-Dikes consist of a normal dike that has a trail dike constructed parallel to the flow from the tip. The constructed trail dike continues the constriction of the channel further along the main channel to increase main channel energy and decrease deposition. The area behind the L-Dike becomes a slack water area with beneficial habitat characteristics. This area can be prone to deposition due to the low energy level within the dikes, but such deposition can be reduced by notching the trail dike so that periodic sediment flushing occurs. Some disadvantages of L-Dikes are that they isolate the bankline from the river channel and that they don't
 promote new bathymetric diversity.


Multiple Roundpoint Structures (MRS) - Multiple Roundpoint Structures induce scouring off the tips of the structures and create depositional areas with the increased roughness generated by the structures. The MRS can also act as a primitive bank stabilization technique by creating depositional zones near the banks of the structures. The structures are generally built to $2 / 3$ bankfull and the grade of stone needed is channel dependent. The spacing of the MRS is dependent of the height of the structure and natural angle of repose of the rock used. A rule of thumb with the spacing between the structures is to space them no less than $2 / 3$ of the height. MRSs can be designed as a single row or in multiple rows. Preliminary data shows that incorporating more rows generates increased bathymetric changes. MRSs are not recommended as a bank stabilization technique but can be incorporated with other forms of bank stabilization such as revetment. The data collected suggest that MRS are providing useful and valuable habitat for a variety of riverine fishes. Collection of blue suckers may indicate these structures are providing a unique habitat type, once more common in the river.

Notched Dikes - Many rock dikes with notches in them can continue to have the same effect on navigation dimensions as un-notched dikes while also promoting increased bathymetric variation. Notches in the center or bank side of dikes achieve this variation by promoting scour downstream of the notch leading to a diversity of habitat. Varying notch depth is one factor that can be used to alter the depth of scour and thus the diversity. Low energy areas behind the un-notched portions of dikes can lead to deposition, supporting the creation of islands

or side channels when used in a
 series. Notching is not always recommended; notching does remove a portion of the dike that may be necessary for the dike to have its intended effect, and a notch may have little effect without the proper flow depth and frequency through the notch.

Off-Bankline Revetment - Off-Bankline Revetment reduces erosion on the shallow side of a river. By constructing a stone structure parallel to the bankline, a small side channel area is formed that is largely cut off from the energy of the main channel, producing a slow water habitat area. There is little critical bathymetric effect as the revetment is placed in shallow areas. However, the use of off-bankline revetment does not guarantee the same level of protection as normal revetment and leaves the bankline exposed at higher flow events.


Rootless Dikes - Rootless dikes function much like notched dikes; they can have the intended effect of redirecting flow in beneficial directions while promoting bathymetric and habitat diversity in the space between the dike and the bank. Rootless dikes are also like notched dikes in that they need to obstruct enough of the flow to have their desired effect, they need to cause a constriction of the flow, and they need the gap between the dike and the bankline to experience the proper flow depth and frequency to have an effect.


Side Channel Enhancement Dike - Side Channel Enhancement Dikes (SCEDs) are a special class of LDikes with the trail oriented upstream from a spur dike constructed on the island side of a side channel entrance. With the upstream-oriented trail, the SCED captures flow from the main channel and redirects it down a side channel, increasing the energy in the side channel, scouring out deposited sediment, and preventing further sedimentation in the side channel. Under the right conditions, the installation of a SCED can reopen closed
side channels, once again providing aquatic habitat in areas it had previously existed. The construction of a SCED does require certain conditions to be met for a higher likelihood of success: 1) a SCED works best when it can be constructed on the channel-dominant bank, and 2) SCED design requires a careful balance of flow capture between the side channel and main channel to avoid sedimentation in either channel.


Stepped-Up Dikes - Stepped-Up dike fields of various elevations were developed to provide an additional element of diversity. They counteract sediment deposition, thereby preventing the conversion of aquatic environment into terrestrial. In the stepped-up dike configuration, each dike in sequence rises two feet higher than the previous one. This approach utilizes the river's energy to change the sediment deposits as the water level rises and falls. When the river's current hits the first dike it is propelled toward the main channel. As the river level rises, it moves over the first dike and hits the second dike, once again moving back into the main channel. This process repeats itself as the river rises and falls. The river's current, moving over each submerged dike, allows the sediment buildup to be redistributed back into the main channel and carried downstream.


W-Dikes - W-Dikes function in a manner very similar to chevrons, but are constructed to act over a larger width of the channel. By using a W-Dike instead of a chevron, two plunge pools are created between the inside and outside legs of the W , with deposition typically occurring downstream of the center of the W. Disadvantages of W-Dike construction include the cost of construction (as they require 2-3 times the stone), the difficulty in construction, and the channel width and depth needed.


Woody Debris - Naturally occurring large woody debris (LWD) (i.e., $>10 \mathrm{~cm}$ diameter and 2 m in length) is an important component of many lotic systems. It provides roughness, reducing velocities and providing overhead cover for fishes, substrate for aquatic invertebrates, and can be an important source of particulate organic matter adding to primary productivity of a river. Large woody debris dissipates flow energy, resulting in channel stability and improved fish migration. It also provides basking and perching sites for reptiles and birds. Placing LWD into streams is an increasingly popular technique to improve fish and wildlife habitat. Large woody debris projects can be divided into two categories: improving the habitat by increasing the amount of LWD in the
stream, and using LWD to alter flow in some way to improve aquatic habitat. Some specific objectives that can be accomplished by using LWD are the following: create pool habitat, generate scour, increase depths through shallow reaches, divert flows away from the bank to reduce erosion, armor stream banks to reduce erosion, promote bar formation through induced sediment deposition, and increase instream cover and refugia. Large woody debris commonly placed into the streams can be categorized as three types: whole trees, logs, and root wads. The use of woody bundles is more common in side channel rehabilitation and streambank stabilization, but can be implemented in dike structures in river environments. A primary concern with the installation of woody debris is that it can have a short life in the field.


Wood Pile Structures - Prior to the 1960's almost all of the structures placed in the Middle Mississippi River were of the woody pile type. Logs were driven into the river bed to create roughness and formed into a river training structure. Due to the higher maintenance of these woody structures, river training structures began to be constructed from stone during the 1960s. There is currently a push to start bringing back the woody pile structures because of their benefit to the micro- and macro-invertebrate species. While wood pile structures promote bathymetric diversity, they are not as effective as stone dike structures for maintaining the navigation channel.

## APPENDICES

## Appendix A

A-1. 22 Reaches Diagram
A-2. Middle Mississippi Water Surface Profiles
A-3. Middle Mississippi Bankline and Navigation Channel Widths
A-4. Bankline and Navigation Channel Widths in Each Reach
A-5. Table of Average Structures per River Mile in Each Reach
A-6. Table of Average Side Channel Miles per River Mile in Each Reach
A-7. Average Structures and Side Channel Miles per River Mile in Each Reach
A-8. Table of Average Notches per River Mile and per Structure Total in Each Reach
A-9. Average Number of Notched Structures per River Mile in Each Reach
A-10. Average Number of Notched Structures per Structure Total in Each Reach

## Appendix B

1. Map of Reach 1, Mel Price Tailwater
2. Map of Reach 2, Mosenthien
3. Map of Reach 3, St. Louis Harbor
4. Map of Reach 4, Cliff Cave
5. Map of Reach 5, Kimmswick
6. Map of Reach 6, Herculaneum
7. Map of Reach 7, Calico/Osborne
8. Map of Reach 8, Salt Lake
9. Map of Reach 9, Fort Chartres
10. Map of Reach 10, Ste. Genevieve
11. Map of Reach 11, Kaskaskia
12. Map of Reach 12, Mile 100 Islands
13. Map of Reach 13, Red Rock to Tower Rock
14. Map of Reach 14, Big Muddy
15. Map of Reach 15, Trail of Tears
16. Map of Reach 16, Schenimann/Picayune
17. Map of Reach 17, Cape Girardeau
18. Map of Reach 18, Thebes
19. Map of Reach 19, Prices
20. Map of Reach 20, Dogtooth
21. Map of Reach 21, Thompson
22. Map of Reach 22, Cairo

Appendix A-1: 22 Reaches Diagram


\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
11-Kaskaskia \\
Field 1 - RDB - High \\
Field 2 - LDB - Medium \\
Field 3 -RDB - Low \\
Field 4 - RDB - Medium
\end{tabular} \& \begin{tabular}{|l|}
\hline 118 \\
117 \\
116 \\
115 \\
114 \\
113 \\
112 \\
111 \\
110 \\
\hline 109 \\
\hline
\end{tabular} \& 1
1
1

3
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4 \& Kasky \& 2,210,101 \& \& 2
2
2
2 \&  \& <br>
\hline \& 109 \& \& \& \& \& \& \& <br>

\hline | 12-Mile 100 Islands |
| :--- |
| Field 1 - RDB - Medium |
| Field 2 - LDB - Medium |
| Field 3 - LDB - Medium |
| Field 4 - RDB - Medium | \& 108

107
106
105
104
103
102
101
100
99
98
97
96 \& 1
1
1
1
1
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4
4
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4

4 \& | Crains |
| :--- |
| Mile 100 |
| Jones | \& 7,220,966 \& Liberty \& 2

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3
3 \&  \& <br>

\hline | 13-Red Rock to Tower Rock |
| :--- |
| Field 1 - LDB - Low |
| Field 2 - RDB - Medium |
| Field 3 - LDB - Medium |
| Field 4-RDB - Medium | \& | 94 |
| :--- |
| 93 |
| 92 |
| 91 |
| 90 |
| 89 |
| 88 |
| 87 |
| 86 |
| 85 |
| 84 |
| 83 |
| 83 |
| 82 |
| 81 |
| 80 |
| 79 | \& 4 \& Owl Creek \& 1,870,202 \& \& \[

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& 3 \\
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\] \&  \& <br>

\hline | 14-Big Muddy |
| :--- |
| Field 1 - LDB - Low |
| Field 2 - LDB - High |
| Field 3 - RDB - Low | \& | 79 |
| :--- |
| 78 |
| 77 |
| 76 |
| 75 |
| 74 |
| 73 |
| 72 |
| 71 | \& 3 \& Cottonwd \& 2,241,165 \& Crawford \& | 1 |
| :--- |
| 2 |
| 2 |
| 2 |
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\hline | 15-Trail of Tears |
| :--- |
| Field 1 - LDB - High |
| Field 2 - RDB - Medium |
| Field 3 - RDB - High | \& | 70 |
| :--- |
| 69 |
| 68 |
| 67 |
| 66 |
| 65 |
| 64 |
| 63 | \& | 2 |
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| 2 |
| 3 |
| 3 |
| 3 |
| 3 |
| 3 | \& \& 2,929,416 \& Vancil \& | 1 |
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| 1 |
| 1 | \&  \& <br>


\hline | 16-Schenimann / Picayune |
| :--- |
| Field 1 - LDB - Medium |
| Field 2 - RDB - High |
| Field 3 - LDB - Low |
| Field 4-RDB - Low | \& | 62 |
| :--- |
| 61 |
| 60 |
| 59 |
| 58 |
| 57 |
| 56 |
| 55 |
| 54 | \& 4 \& Schenimn \& 2,558,436 \& Picayune \& \[

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\end{aligned}
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\] \&  \& <br>

\hline | 17-Cape Girardeau |
| :--- |
| Field 1 - RDB - High |
| Field 2 -RDB - Low |
| Field 3 - LDB - Medium | \& | 53 |
| :--- |
| 52 |
| 51 |
| 50 |
| 49 |
| 48 |
| 47 |
| 46 | \& 2 \& \& 1,152,438 \& Marquette \& 3 \& \[

\hat{5}
\] \& <br>

\hline | 18-Thebes |
| :--- |
| Field 1-RDB - Low |
| Field 2 - LDB - High |
| Field 3 - RDB - Low |
| Field 4 - LDB - Low | \& | 45 |
| :--- |
| 44 |
| 43 |
| 42 |
| 41 |
| 40 |
| 39 |
| 38 |
| 37 |
| 36 |
| 35 | \& 1

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3 \& \& 3,076,552 \& | Thebes |
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| Sante Fe | \& 2

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Appendix A-5: Table of Average Structures per River Mile in Each Reach

| Reach | Reach Name | $\begin{gathered} \hline \text { RM } \\ \text { Start } \end{gathered}$ | RM End | Total Miles | RDB Dikes | Avg. RDB <br> Dikes/RM | LDB <br> Dikes | Avg. LDB <br> Dikes/RM | Chevrons | Avg. <br> Chevrons / RM | TOTAL Struc. | Average <br> Structures / RM |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Mel Price Tailwater | 201 | 196 | 5 | 5 | 1.0 | 0 | 0.0 |  | 0.0 | 5 | 1.0 |
| 2 | Mosenthien | 196 | 184 | 12 | 1 | 0.1 | 11 | 0.9 |  | 0.0 | 12 | 1.0 |
| 3 | St. Louis Harbor | 184 | 168 | 16 |  | 0.0 | 14 | 0.9 | 3 | 0.2 | 17 | 1.1 |
| 4 | Cliff Cave | 168 | 163.5 | 4.5 | 12 | 2.7 | 10 | 2.2 |  | 0.0 | 22 | 4.9 |
| 5 | Kimmswick | 163.5 | 156.5 | 7 | 4 | 0.6 | 23 | 3.3 | 7 | 1.0 | 34 | 4.9 |
| 6 | Herculaneum | 156.5 | 149.5 | 7 | 12 | 1.7 | 18 | 2.6 |  | 0.0 | 30 | 4.3 |
| 7 | Calico / Osborne | 149.5 | 143 | 6.5 | 16 | 2.5 | 16 | 2.5 |  | 0.0 | 32 | 4.9 |
| 8 | Salt Lake | 143 | 134.5 | 8.5 | 11 | 1.3 | 27 | 3.2 |  | 0.0 | 38 | 4.5 |
| 9 | Fort Chartres | 134.5 | 128 | 6.5 | 6 | 0.9 | 14 | 2.2 | 2 | 0.3 | 22 | 3.4 |
| 10 | St. Genevieve | 128 | 119.5 | 8.5 | 15 | 1.8 | 21 | 2.5 |  | 0.0 | 36 | 4.2 |
| 11 | Kaskaskia | 119.5 | 109.5 | 10 | 35 | 3.5 | 18 | 1.8 |  | 0.0 | 53 | 5.3 |
| 12 | Mile 100 Islands | 109.5 | 95 | 14.5 | 48 | 3.3 | 17 | 1.2 | 7 | 0.5 | 72 | 5.0 |
| 13 | Red Rock to Tower Rock | 95 | 80 | 15 | 18 | 1.2 | 26 | 1.7 | 4 | 0.3 | 48 | 3.2 |
| 14 | Big Muddy | 80 | 71 | 9 | 7 | 0.8 | 31 | 3.4 |  | 0.0 | 38 | 4.2 |
| 15 | Trail of Tears | 71 | 62.5 | 8.5 | 23 | 2.7 | 32 | 3.8 |  | 0.0 | 55 | 6.5 |
| 16 | Schenimann / Picayune | 62.5 | 54 | 8.5 | 25 | 2.9 | 24 | 2.8 |  | 0.0 | 49 | 5.8 |
| 17 | Cape | 54 | 46 | 8 | 3 | 0.4 | 16 | 2.0 |  | 0.0 | 19 | 2.4 |
| 18 | Thebes | 46 | 35 | 11 | 27 | 2.5 | 23 | 2.1 | 4 | 0.4 | 54 | 4.9 |
| 19 | Prices | 35 | 29 | 6 | 6 | 1.0 | 10 | 1.7 | 3 | 0.5 | 19 | 3.2 |
| 20 | Dogtooth | 29 | 20 | 9 | 12 | 1.3 | 19 | 2.1 | 1 | 0.1 | 32 | 3.6 |
| 21 | Thompson | 20 | 12 | 8 | 7 | 0.9 | 23 | 2.9 |  | 0.0 | 30 | 3.8 |
| 22 | Cairo | 12 | 0 | 12 | 13 | 1.1 | 29 | 2.4 |  | 0.0 | 42 | 3.5 |
|  |  |  |  | 201 | 306 | 1.5 | 422 | 2.1 | 31 | 0.2 | 759 | 3.8 |

Appendix A-6: Table of Average Side Channel Miles per River Mile in Each Reach



Appendix A-8: Tables of Average Notches per River Mile and per Structure Total in Each Reach




Legend
=_ Structure degradation
工_Dikes since 2002
$\qquad$ Wood Piles
EL. 10
EL. 0
EL. -10
EL. -20
EL. -30

```
555,000
```

560,000
565,000
570,000
580,000
575,000
585,000
590,000
595,000
600,000

## Legend

—Structure degradation
_ Structures since 2002
_ Wood Piles
EL. 10
EL. 0
EL. -10
$\square$ EL. -20
EL. -30


US Army Corps of Engineers ${ }^{\text {a }}$
St. Louis District

## Legend

=Structure degradation
工 Structures since 2002
——Wood Piles
EL. 10
EL. 0
EL. -10
EL. -20
EL. -30
$550,000 \quad 555,000$

| U.S. ARMY ENGINEER DIVISION CORPS OF ENGINEERS ST. LOUIS, MISSOURI |
| :---: |
| MISSISSIPPI RIVER BASIN <br> 2010 River Survey <br> 2011 Side Channel Survey $\qquad$ |

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St. Louis District

## Legend

= Structure degradationStructures since 2002
Wood Piles
EL. 10
EL. 0
EL. -10
EL. -20
EL. -30


| PLATE <br> NUMBER |  |  |  |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
|  | REACH 6 <br> HERCULANEUM |  |  |


| U.S. ARMY ENGINEER DIVISION CORPS OF ENGINEERS ST. LOUIS, MISSOURI |
| :---: |
| MISSISSIPPI RIVER BASIN 2010 River Survey 2011 Aerial Photography |



## Legend

$=$ Structure degradation
Structures since 2002
Wood Piles
EL. 10
EL. 0
EL. -10
EL. -20
EL. -30

| $535,000$ | $540,000$ | $545,000$ |
| :---: | :---: | :---: |
| PLATE NUMBER |  | U.S. ARMY ENGINEER DIVISION CORPS OF ENGINEERS ST. LOUIS, MISSOURI |
|  | REACH 7 <br> CALICO / OSBORNE | MISSISSIPPI RIVER BASIN 2010 River Survey 2011 Side Channel Survey 2011 Aerial Photograph |

560,000


## Legend

= Structure degradation
Wood Piles

EL. 10
$\square$ EL. 0
EL. -10
$\square$ EL. -20
EL. -30

## 590,000

| PLATE |
| :---: |
| NUMBER |
| 0 |


|  |  |  |
| :---: | :---: | :---: |
|  |  |  |
| REACH 9 <br> FT. CHARTRES |  |  |


| U.S. ARMY ENGINEER DIVISION CORPS OF ENGINEERS ST. LOUIS, MISSOURI |
| :---: |
| $\begin{aligned} & \text { MISSISSIPPI RIVER BASIN } \\ & 2010 \text { River Survey } \\ & \text { 2011 Side Channel Survey } \\ & 2011 \text { Aerial Photography } \end{aligned}$ |

610,000


690,000




| PLATE <br> NUMBER |
| :---: |
| 14 |



800,000
805,000



Legend

| $=$ | Structure degradation |
| ---: | :--- |
| $=$ | Structures since 2002 |
|  | Wood Piles |
|  | EL. 10 |
|  | EL. 0 |
|  | EL. -10 |
|  | EL. -30 |


| 795,000 800,000 |  | 805,000 |
| :---: | :---: | :---: |
| PLATE NUMBER$18$ |  | U.S. ARMY ENGINEER DIVISION CORPS OF ENGINEERS st. louis, missouri |
|  | REACH 18 THEBES | MISSISSIPPI RIVER BASIN <br> 2010 River Survey <br> 2011 Side Channel Surve <br> 2011 Aerial Pho |


$=$
$=$
$=$
Structure degradation

EL. 10

EL. 0

EL. -10

EL. -20

EL. -30


| U.S. ARMY ENGINEER DIVISION <br> CORPS OF ENGINEERS ST. LOUIS, MISSOURI |
| :---: |
| MISSISSIPPI RIVER BASIN <br> 2010 River Survey 2011 Side Channel Survey <br> 2011 Aerial Photograph |

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 of EngineersSt. Louis District
$=$ Structure degradation
$\overline{=}$
$=$ Structures since 2002

EL. 10

EL. 0

EL. -10

EL. -20
EL. -30
(1)

855,000
N $\longrightarrow 2$

|  |  |  |
| :---: | :---: | :---: |
|  |  |  |
| REACH 21 |  |  |


| U.S. ARMY ENGINEER DIVISION CORPS OF ENGINEERS ST. LOUIS, MISSOURI |
| :---: |
| MISSISSIPPI RIVER BASIN 2010 River Survey 2011 Side Channel Survey 2011 Aerial Photography |

US Army Corps of Engineers ©

## Legend

LStructure degradation


Wood Piles
EL. 10
EL. 0
EL. - 10
EL. -20
EL. -30

| 865,000 | 870,000 | 875,000 880 |  | 885,000 | 890,000 | 895,000 | 900,000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PLATE NUMBER$22$ |  | U.S. ARMY ENGINEER DIVISION CORPS OF ENGINEERS <br> ST. LOUIS, MISSOURI | $\begin{gathered} N \\ 4 \end{gathered}$ |  |  |  |  |
|  | REACH 22 CAIRO | MISSISSIPPI RIVER BASIN 2010 River Survey 2011 Side Channel Survey 2011 Side Channel Survey |  |  |  |  | US Army Corps of Engineers * <br> St. Louis District |

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[^0]:    ${ }^{1}$ Lauth et. al., "Analysis of the Effects of Bendway Weir Construction on Channel Cross-Sectional Geometry", 2011

